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TYPOLOGICAL ANALYSIS AND VULNERABILITY CURVES FOR MASONRY CHURCHES

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Abstract

Masonry churches have a high intrinsic seismic vulnerability, demonstrated by the effects of the last earthquakes in Italy. In the present study a database of 1391 II level post-earthquake survey form (A-DC) has been analyzed. The forms were filled by the University of Padua, the University of Naples Federico II and the University of Naples Parthenope, under the coordination of the Department of Civil Protection, the Cultural Heritage Ministry (MiBACT) and the Italian Laboratories University Network of Seismic Engineering (Re-LUIS). The form were filled after the 2016/2017 Central Italy seismic sequence (889 forms), the 2012 Emilia earthquake (264 forms) and after the 2009 L'Aquila earthquake (238 forms). A typological investigation has been done as preliminary phase, and some vulnerability modifiers have been determined, with the aim of developing vulnerability and fragility curves dependent of poor but effective typological characteristics of the buildings.

Keywords: Masonry Churches, Definition of Typologies, Vulnerability Curves, L'Aquila 2009, Emilia 2012, Central Italy 2016.

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1 INTRODUCTION

In the last decades, great losses have occurred to the artistic and cultural heritage as a result of seismic events. In particular, serious damage has been suffered by churches [1-6], object of the present study. With the purpose of assess the safety conditions and collect the data of the damage suffered by ecclesiastical buildings, a specific form for the survey of damage churches [7, 8] was developed. The current version (A-DC form [9, 10]) consists of several sections, in which identification data, context description, damage data, safety evaluations and basic geometric information of the building are reported. As concern the damage survey, the form is based on the identification of the damage level (from 0 to 5) of 28 possible collapse mechanisms of macro-elements. Then, it is possible to obtain an overall damage index i_d (from 0 to 1) as a normalized average of the damage level of each mechanism.

The seismic events considered in this study are those in which the form for the damage survey of churches has been used in its actual version: the 2009 L'Aquila earthquake, the 2012 Emilia earthquake and the 2016/17 Central Italy seismic sequence. The surveys have been carried out under the coordination of the Department of Civil Protection (DPC) and the Ministry of Cultural Heritage and Tourism (MiBACT) by group of technicians (structural engineers, officials of the superintendence, fireman if the safety level was low). In particular, the authors have used A-DC forms filled mainly by the University of Padua, and in part by the University of Naples Federico II and the University of Naples Parthenope.

Churches are a peculiar type of building which has intrinsic seismic vulnerability due to its constructive and typological features (i.e. great lights, absence of intermediate diaphragms, large height to width ratio of walls, thrusting horizontal structures) [11]. Thus, in order to elaborate large-scale analysis, churches must be approached differently than ordinary buildings [2, 13, 14]. Usually, the evaluation of seismic risk at territorial scale requires the identification of different classes of buildings which have similar behavior [12]. For ordinary buildings, those classes are generally defined by the type of load-bearing structure (e.g. masonry, reinforced concrete, etc.) and by the constructive techniques and building regulations (mainly identifying with age of construction ranges). On the other hand, churches are usually load-bearing masonry buildings, distinguished by typological features more than constructive ones (e.g. presence of macro-elements, type of plan and façade, etc.). Therefore, the aim of this work is to identify typological characteristics that affect the vulnerability of the churches, in order to allow the elaboration of typological vulnerability and fragility curves that could account for different churches vulnerabilities and therefore be applied on large-scale seismic risk assessment according to the churches features.

2 TYPOLOGICAL DESCRIPTION OF THE SAMPLE

The database considered in the present study includes a total of 1391 post-earthquake survey A-DC forms [9, 10], filled mainly by the University of Padua, and in part by the University of Naples Federico II and the University of Naples Parthenope. Of these, 889 were collected following the 2016/2017 Central Italy earthquake sequence [6], 264 following the 2012 Emilia earthquake [4], and finally 238 following the 2009 L'Aquila earthquake [3]. Table 1 shows the geographical distribution of the surveys.

As already mentioned, in order to carry out the vulnerability analysis of churches it is necessary to consider the great geometrical and typological differences that they may present, which could lead to a very different seismic response. In particular, using the information collected from the A-DC forms and the photos of the post-earthquake surveys, the typological distributions of the churches affected by the three 2009, 2012 and 2016/17 earthquakes have been analyzed.

Earthquake	Regions (number of churches): province
Central Italy 2016/17	Marche (602): Ancona (AN), Ascoli Piceno (AP), Fermo (FM), Macerata
	(MC), Pesaro e Urbino (PU)
	Abruzzo (111): L'Aquila (AQ), Chieti (CH), Pescara (PE), Teramo (TE)
	Umbria (110): Perugia (PG), Terni (TR)
	Lazio (66): Frosinone (FR), Rieti (RI), Viterbo (VT)
Emilia 2012	Emilia Romagna (138): Bologna (BO), Ferrare (FE), Modena (MO), Reggio
	Emilia (RE)
	Lombardia (82): Cremona (CR), Mantova (MN)
	Veneto (44): Rovigo (RO)
L'Aquila 2009	Abruzzo (238): L'Aquila (AQ), Teramo (TE)

Table 1: Geographical distribution of the sample.

Specifically, the distribution of the following database parameters was studied [6]: a) type of plan (Figure 1); b) type of façade; c) masonry type; d) type of bell structure; and e) dimensions (volume).

The results in terms of the distribution of the analyzed features are collected in Table 2 and the typologies associated with each church belonging to the database, geographically located, are presented in Figure 2.

As regards to the type of plan, seven types were identified based on the number of naves, the presence of apse, transept and side chapels (Figure 1). Specifically: type 1 represents one nave churches with, simple rectangular plan, without apse or aggregated elements; type 2 is similar to type 1, with the addition of the apse; type 3 represents the most complex possibility for one nave churches (apse, transept and/or side chapels); type 4 is three or more naves church, with very complex plan (transept, chapels, apses at the end of naves and transept); type 5 is also a three or more naves church, with medium complex plan; type 6 represents the less complex typology of three naves churches (includes also the 2 naves churches); type 7 is circular or central plan (polygonal) church.

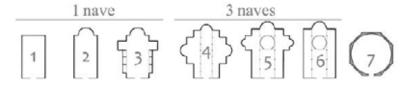


Figure 1: Schematic representation of the seven type of plan considered in this study.

The analysis of the sample showed that in Central Italy simpler churches are predominant. The most common types are 1 and 2, whereas with very small percentages are found types 3, 5 and 6; types 4 and 7 are just over 1%. Table 2 and Figure 2 show that the churches affected by the 2009 L'Aquila earthquake have many similarities with the ones of the 2016/17 Central Italy seismic sequence (both affect the central Apennine belt). In fact, the most widespread are type 1 and 2 churches (82.8 % CI and 66.9% AQ), but also, type 6 and type 3 are common. The trend identified in the Central Italy region changes considerably for the churches located in the Po Valley: the percentage of type 1 is very small (mostly oratories and minor private chapels). Instead, the more complex typologies (type 3, 6 and 5) are more widespread with a cumulative percentage of 61.4%. The numbers of types 4 and 7 remain marginal. Analyzing the geographical distribution, it can be observed that in the Apennine region there is a predominance of single nave churches (mainly typologies 1 and 2); the cases of churches with more naves are located in the less mountainous areas and in Abruzzo, and they belong to typology 6, so they

have a not excessively complex geometry. In the Po Valley the typologies present are distributed in the territory, and are not visibly dependent on geographical location.

The second feature analyzed is the type of façade. Four main types of façade have been identified: gabled, salient façade, quadrangular and polygonal. The cases that was not possible to trace back to one of these four types (e.g. churches with side entrances connected to adjacent buildings on several sides or churches with a large prothyrum or narthex) were excluded from the present analysis, because of the different seismic behavior of the façade macroelement.

With regard to the sample of Central Italy, there is a clear majority of gabled type, whereas the church façades of the L'Aquila earthquake belong in large part to the gabled and the quadrangular type. Instead, most of the churches in the Po Valley have salient and gabled façades.

The type of façade seems to have no correlation with geographical location (Figure 2) probably due to similar geographical conditions of the inspected area all enclosed in the plain.

Another important typological characteristic is the masonry type. Since the masonry texture is often covered by plaster, it is not always possible to determine the constituent material of the walls, unless more in-depth investigations are carried out. As for the façade, also for the masonry typology, the not identified cases have been excluded from the typological analysis.

Four masonry types have been distinguished: random stone, stone ashlar, brick masonry and mixed stone and brick masonry. The masonry parameter distribution is the most clearly readable: in Central Italy and L'Aquila samples, stone is the most common material (mainly random rubble), whereas in Emilia no cases of stone masonry but an almost totality of brick masonry have been identified. Figure 2 shows that the type of masonry depends almost exclusively on the geographical/topographical location. In the lowland areas and in the coastal strip only brick masonry (or mixed masonry at most) is present, whereas rising to a higher altitude and moving away from the coast, bricks begin to be flanked by the stone until it is completely replaced by it (this is particularly evident in the Central Italy earthquake).

Regarding the type of bell tower, four types have been identified: isolated bell tower, bell tower integrated or partially integrated with the church structure, bell gable and absence of bell tower. The samples of Central Italy and L'Aquila have similar distributions: the most common types are integrated bell tower and bell gable, whereas isolated bell tower is very uncommon. L'Aquila sample has also a 10% of cases in which the bell tower is absent. Also, for this parameter, the Emilia database is visibly different from the others, presenting for the most part integrated and isolated bell tower, and only few cases of bell gable. Figure 2 shows that, in this case, the differences between the distributions of the samples depend more on the territorial/regional area, rather than on altimetric or topographical factors.

The last of the typological features analyzed is the volume of the church. Since many forms were incomplete in the section related to the geometric survey, also this parameter is not identified for the all database. Six ranges of volume have been chosen: two ranges of very small and small churches (from 0 to 250 and from 250 to 500 m³), two of medium size churches (from 500 to 1000 and from 1000 to 2500 m³) and two ranges of large churches (from 2500 to 5000 and from 5000 m³ upwards). Table 2 shows that in Central Italy and L'Aquila the most widespread churches are those of medium size, followed by small churches and lastly those of large size. Instead, in Emilia, the most of the churches have a large or medium volume. From a territorial distribution point of view, large churches are typically located in lowland areas or in correspondence of cities or important centers (Figure 2).

	Central Italy 2016/17		L'Aquila 2009		Emilia 2012	
	n	%	n	%	n	%
Churches	889		238		264	
Plan shape						
1	322	42.0%	103	43.6%	25	9.5%
2	313	40.8%	55	23.3%	71	26.9%
3	43	5.6%	29	12.3%	81	30.7%
4	13	1.7%	0	0.0%	5	1.9%
5	26	3.4%	8	3.4%	30	11.4%
6	38	5.0%	40	16.9%	51	19.3%
7	12	1.6%	1	0.4%	1	0.4%
sum	767	86.3%	236	99.2%	264	100.0%
Façade typology						
Gabled	572	74.4%	100	47.2%	104	41.8%
Salient	65	8.5%	16	7.5%	122	49.0%
Quadrangular	74	9.6%	71	33.5%	2	0.8%
Polygonal	58	7.5%	25	11.8%	21	8.4%
sum	769	86.5%	212	89.1%	249	94.3%
Masonry typology						
Random stone	318	43.6%	95	60.1%	0	0.0%
Stone ashlar	52	7.1%	30	19.0%	0	0.0%
Stone/Brick	141	19.3%	27	17.1%	2	0.9%
Brick	219	30.0%	6	3.8%	229	99.1%
sum	730	82.1%	158	66.4%	231	87.5%
Bell tower typology						
Bell tower isolated	17	2.5%	5	2.2%	63	24.0%
Bell tower integrated	351	52.5%	73	31.9%	146	55.5%
Bell gable	283	42.3%	127	55.5%	11	4.2%
No bell tower	18	2.7%	24	10.5%	43	16.3%
sum	669	75.3%	229	96.2%	263	99.6%
Volume [m³]						
0 - 250	100	12.7%	22	18.6%	14	6.1%
250 - 500	131	16.6%	17	14.4%	17	7.5%
500 - 1000	183	23.3%	28	23.7%	11	4.8%
1000 - 2500	185	23.5%	32	27.1%	47	20.6%
2500 - 5000	94	11.9%	12	10.2%	61	26.8%
> 5000	94	11.9%	7	5.9%	78	34.2%
sum	787	88.5%	118	49.6%	228	86.4%

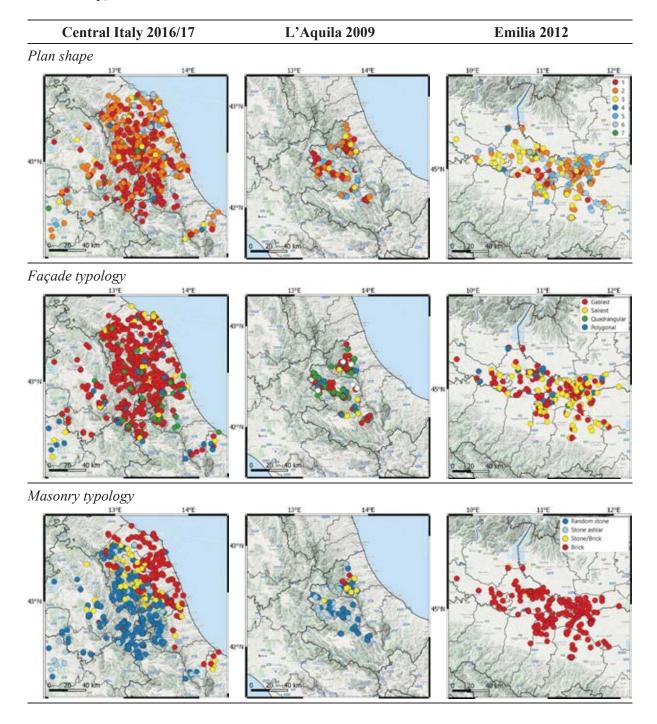
Table 2: Statistical distribution of plan shape, façade type, masonry type, bell tower typologies and volume for the earthquake of Central Italy 2016/17, L'Aquila 2009 and Emilia 2012.

It can be concluded that Emilia churches are typologically very different from Central Italy and L'Aquila ones. The latter, belonging to the same geographical area, have more homogeneous characteristics, with some differences due to the proximity to the coast and to altimetric/topographical factors. In particular, the feature that the most depends on altitude is the masonry type, as a direct consequence of the availability of the different materials on site. The other parameters analyzed are not directly dependent on the altimetry, but are more related to the territorial/regional building traditions, especially evident in the type of façade and bell tower.

In summary, it emerges that the churches of Central Italy are mainly simple, medium size and single nave, with a gabled façade and a bell gable or a bell tower integrated into the structure of the church, built in stone (mostly random) in the Apennine area and brick in the coastal strip. Very similar are the churches affected by the L'Aquila earthquake, with the only difference that prefer a quadrangular façade and the cases with more than one nave are more widespread, although maintaining a very simple plan. Very different are the churches of Emilia and the Po

Valley regions, which have large complex plans with gabled or salient façades, with the presence of isolated or integrated bell tower and built almost exclusively in brick.

To compare several features, the maps in Figure 2 show that in Emilia there is a good correspondence between volume and complexity (typology of plan shape), whereas in Central Italy even when the churches are large the complexity is never high (particularly evident on the coastal strip).



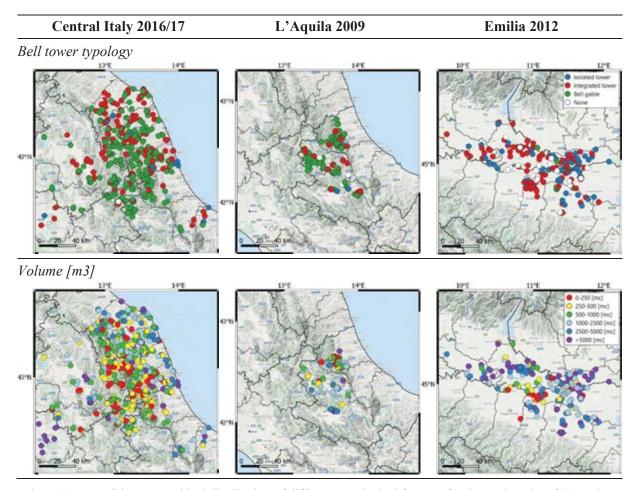


Figure 2: Map of the geographical distribution of different typological features for the earthquake of Central Italy 2016/17, L'Aquila 2009 and Emilia 2012.

3 VULNERABILITY CURVES

The seismic vulnerability of a building is defined as the propensity of the structure to suffer damage after a seismic event of a given intensity. It could be represented by a continuous function called vulnerability curve that relates the expected mean value of damage of a class of buildings to the seismic intensity. The latter is usually presented in terms of macroseismic intensity, but it can also be provided as peak ground acceleration-PGA values.

The formulation originally provided by [15] for residential buildings and further adapted to churches by Lagomarsino and Podestà [13] (1) was take as reference to develop typological vulnerability curves.

$$\mu_d = 2.5 \left[1 + \tanh\left(\frac{I + 3.4375 \cdot \overline{\iota_v} - 8.9125}{g}\right) \right] \tag{1}$$

where μ_d represents the mean damage grade ($0 \le \mu_d \le 5$) as function of: the macroseismic intensity *I* expressed in accordance with the MCS scale [16], the mean vulnerability score i_v derived from the second level survey form for churches [17], and the ductility index q = 3.

In particular, a fitting procedure of the observational damage data collected was carried out using (2):

$$\mu_D = 2.5 \cdot [1 + \tanh(\alpha \cdot I_{MCS} + \beta)] \tag{2}$$

with
$$\alpha = 1/q$$
 (3)

and
$$\beta = a \cdot i_v + b$$
 (4)

and optimizing the value of α and β .

The formulation (2) is equivalent to (1), but expressed in terms of the two parameters α (3) and β (4),. In this way, from the fitting procedure on mean damage values, the resulting vulnerability curve inherently includes the average value of i_{ν} on the whole dataset. Indeed, as suggested below, the evaluation of different vulnerabilities classes or typologies could be related to a selected subset of homogenous churches.

3.1 Consideration on the damage index i_d

As mentioned before, the A-DC survey form allows to calculate an overall damage score (damage index) i_d for each church. In particular:

$$i_d = \frac{1}{5} \frac{\sum_{k=1}^n d_k}{n} \tag{5}$$

where n is the number of mechanisms that can be potentially activated in the church and d_k is the damage recorded in the k-th mechanism (from 0 to 5).

In order to be used for vulnerability and fragility analysis, the damage index i_d has to be converted to a damage level from 0 to 5, according to the EMS scale [18]. One of the most used correlation [13] is reported in Table 3.

Damage index i _d	0-0.05	0.05-0.25	0.25-0.4	0.4-0.6	0.6-0.8	0.8-1
Damage level (EMS98)	DS0	DS1	DS2	DS3	DS4	DS5
Description of the damage	no damage	slight damage	moderate damage	heavy damage	very heavy damage	collapse

Table 3: Correlation between the damage index id of the A-DC form and the damage level according to the EMS98 scale [13].

Using the correlation in Table 3, a process of discretization of a continuous quantity is carried out. This process is required to relate the result of the A-DC form to a damage level and to build damage probability matrices (DPM), but inevitably, it implies a great loss of detail. Moreover, this discretization slightly varies the overall mean description of the damage. For instance, considering a dataset of 101 churches equally distributed in the damage index i_d from 0 to 1, due to the different dimensions of each damage state, that discretization leads to an average μ_D damage of 2.87 instead of the mathematical mean of 2.50. Figure 3 reports the real case of the 2016/17 Central Italy database with i_d multiplied by 5 to have a comparison. The graph shows how different the damage results can be: as expected, in general the mean damage obtained through the correlation proposed by Lagomarsino and Podestà [13] is higher then that obtained directly by the damage index i_d , but not in a consistent way. Indeed, in correspondence of some intensities (e.g I_{MCS} =8 and I_{MCS} =9.5) the difference is very low (about 0.15), while for others (e.g I_{MCS} =7.5, I_{MCS} =8.5 and I_{MCS} =10) the difference is very impacting (0.5). This is a consequence of the specific distribution of the sample, and therefore it can generate unreliable results in terms of comparison analysis.

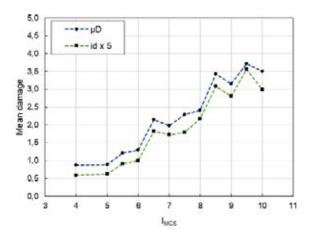


Figure 3: Comparison between the mean value of the damage expressed in terms of μ_D and i_d for the Central Italy churches.

Therefore, since this study works directly on the average damage to figured out the vulnerability curve, and does not use the DPMs, it was decided to build the vulnerability curve in terms of damage index, using in place of the usual mean value μ_d (2) the average i_d values (6):

$$i_d = 0.5 \left[1 + \tanh(\alpha \cdot I_{MCS} + \beta) \right] \tag{6}$$

The value of 2.5 is assumed as 0.5 accordingly to the domain of i_d . This choice has been made both to have more possibilities to adapt the curve to the observational values, and to use in a direct way the information obtained from the damage surveys, avoiding the loss of information deriving from the discretization of the value of i_d .

3.2 Fitting procedure

Once defined the formulation (6), some specification about the adopted fitting procedure are herein reported.

The two coefficients α and β have been calibrated with the minimization of the total error. The ductility related coefficient α was not keep fixed to q=3 since the observation of three different earthquakes and an extended sample shows a variability of this factor as reported in Table 4. As concern the β parameter, it was derived by the mean value of the observational damage indices of the A-DC forms, with a fitting procedure based on the minimization of the total error resulting from the sum of the square residual.

Table 4 reports values obtained from the fitting of eq. (6) and Figure 4 plot each vulnerability curve on the experimental data observed. As is possible to notice there is a good agreement between the observed data and the continuous curves with very limited errors.

	Central Italy 2016/17	L'Aquila 2009	Emilia 2012
α	0.263	0.316	0.360
β	-2.205	-2.678	-2.471
error	9.86 x 10 ⁻⁰⁴	4.83 x 10 ⁻⁰⁴	1.82 x 10 ⁻⁰³
\overline{q}	3.807	3.161	2.778

Table 4: Value defined for the three analyzed earthquakes according to eq. (6)

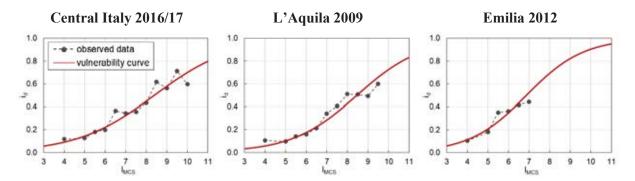


Figure 4: Vulnerability curves obtained from the three analyzed earthquakes

4 INFLUENCE OF TYPOLOGIES

Since the previously observed curves are defined on the whole dataset, hence accounting for the average vulnerability, the selection of homogenous dataset of churches with the same vulnerability may improve the overall evaluation.

Once defined the vulnerability model and the fitting method, it was possible to analyze the influence on seismic vulnerability of different typology characteristics that may lead to the homogenous subset above seek. Specifically, in this paper, the influence of masonry type and the number of naves are presented.

On the basis of the results reached in section 2 about the typological distribution of the churches belonging to the database, the following analyses have been carried out limited to the churches of Central Italy and L'Aquila, in order to guarantee the uniformity of the sample. Future more accurate analysis will allow to study the entire database, and come to overall results not affected by possible errors due to not considered features.

4.1 Influence of masonry type

The first typological parameter to be analyzed is the type of masonry. The categories already identified in the context of typological characterization have been further simplified and reduced to three: stone masonry (both ashlar and random rubble masonry), brick masonry and mixed stone and brick masonry.

Figure 5a shows that the two extreme categories (i.e. stone masonry and brick masonry) have a marked difference in terms of damage, whereas the behavior of the intermediate one (i.e. mixed masonry) seems to be less linear and tends to overlap with the former in correspondence of some I_{MCS}. This can be attributed to the great variability that mixed masonry can presents, sometimes with a predominance of stone, sometimes of brick. Moreover, it is possible that in some cases the particular disposition of the different materials composing the masonry leads to both particularly unfavorable and favorable consequences.

Therefore, this parameter proves to be relevant for the definition of seismic vulnerability. In Figure 5b the results of the fitting procedure are shown. In this elaboration, the behavior of mixed masonry churches emerges to be very similar to stone masonry ones, although those constructed in brick masonry proves to have a much better response to seismic actions.

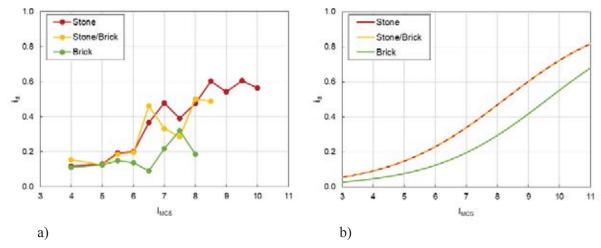


Figure 5: Mean i_d values for stone, mixed (stone/brick) and brick masonry churches (a) and resulting vulnerability curves (b).

4.2 Influence of number of naves

The number of naves is the second typological feature analyzed. In particular, two classes were defined [19, 20]: one nave churches and more than one nave.

Figure 6a shows that for low value of I_{MCS} the damage observed for the two classes is similar. Then, with the increase of the intensity, the different behavior of the different types clearly emerges: churches with more than one nave tend to be less vulnerable compared to those with one nave. The different vulnerability is justified by the greater possibility of churches with several naves to absorb horizontal forces, thanks to the presence of colonnades and more widespread connections. On the other hand, the presence of such elements also makes less likely that all of them are damaged in a marked way; in fact, as the complexity increases, the weight of each macro-element decreases on the overall evaluation of the damage, leading on lower damage indices.

In Figure 6b, the vulnerability curves calibrated on the observed damage of both one and more than one nave churches.

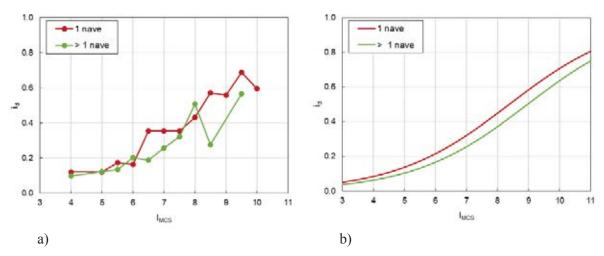


Figure 6: Mean i_d values for one nave and more than one nave churches (a) and resulting vulnerability curves (b).

5 CONCLUSIONS

- The present paper has presented a detailed typological distribution analysis of 1391 churches, affected by the 2009 L'Aquila earthquake, the 2012 Emilia earthquake and the 2016/17 seismic sequence of central Italy. The considered features have been plan shape, type of façade, masonry type, typology of bell tower, and volume of the church. It was figured out that the greater differences are due to the geographical and the altimetric/morphological location. In particular, churches of Central Italy regions are mainly simple, medium size and single nave, with a gabled or quadrangular façade and a bell gable or a bell tower integrated into the structure of the church, built in stone (mostly random) in the Apennine area and brick in the coastal strip. On the contrary, the churches located in the Po Valley regions generally have large complex plans with gabled or salient façades, with the presence of isolated or integrated bell tower and built almost exclusively in brick.
- Then, a methodology to derive vulnerability curves from damage data collected by the A-DC survey forms were defined starting form [13] and adapting the formulation to large scale and typological evaluation needs. Specifically, a reflection on the relation between the damage index i_d and the discrete damage value μ_d was made and the vulnerability curves for the three analyzed earthquakes were provided.
- Lastly, the impact on seismic vulnerability related to the type of masonry and the number of naves of the churches was analyzed. Three different masonry typologies were defined (i.e. stone masonry, brick masonry and mixed stone and brick masonry), with the result that stone masonry and mixed masonry churches have a similar vulnerability, significantly higher than the one of brick masonry churches. Regarding the number of naves, one nave churches result more vulnerable of more than one nave ones, probably thanks to the presence of colonnades and widespread connections.
- Possible future developments are, first of all, the analysis of the influence of more typological parameters on the seismic vulnerability of churches. Then, an important further study is the extension of the procedure to the overall database, inclusive of Emilian churches.

ACKNOWLEDGEMENTS

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