

## INVESTIGATION OF THE IMPACT OF SEISMIC ZONE TO THE COST OF CONSTRUCTION OF A 5-STOREY R/C BUILDING

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### Abstract

*Residing in a country like Greece, where the earthquake is a common phenomenon in most of its areas, the need for constructing earthquake resistant buildings that will provide security and functionality to their residents is imperative. For this reason, the present study estimates the cost of constructing the same five-storey building in three different seismic hazard zones. Initially, this building is studied, in accordance with the provisions of Eurocode 8, for seismic zones I, II and III. The dimensioning and calculation of the weight of the required steel and the volume of the required concrete is carried out. The results from the three seismic zones are presented in detail, both for each structural element of the construction separately and for the whole construction, and a comparison is made between them.*

**Keywords:** Seismic hazard zones, Multi-storey building, Construction's cost, Reinforcement

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## 1 INTRODUCTION

In modern times, various materials are used for the construction of high-rise buildings. The choice of these materials can be made depending on the use of the building, the area in which it is located, the architectural and static study, the cost of construction [1]–[5]. However, in Greece, for the majority of buildings, reinforced concrete is used as a construction material. A reinforced concrete building is made of concrete and steels in the form of rebars or ties. These two materials are harmoniously combined in order, on the one hand, the concrete to receive the compressive forces and on the other hand, the steel to receive the tensile stresses [6], [7]. Greece is an intensely seismic country and as earthquake action is a dangerous and destructive natural phenomenon, the buildings, whether they are new constructions or older, must deal with it effectively. This effective response comes through the design and construction of anti-seismic buildings, but also the strengthening of existing ones [8]–[18].

Nowadays, more and more high-rise buildings are being constructed, with many floors, which are quite sensitive, not only to large earthquakes, but also to less intense ones, if they are not built properly. One of the main problems of these buildings is that, during the earthquake, probably some of their floors move in one direction, while at the same time the other floors move in the opposite direction [19], [20]. Therefore, the engineer should take very seriously the seismic zone in which each building is constructed. The seismic zone significantly affects the dimensioning of the structure, the cross sections of its structural elements and their reinforcement, thus affecting its cost. The engineer has the ability, if for some reason he deems it necessary, to dimension his building in a higher seismic zone than the one to which the building belongs. However, he should not forget that his choice will increase the final construction cost.

The present study presents the simulation and dimensioning, based on modern regulations, of three buildings which have the same standard floor plan, the number of floors (five floors), but are located in different seismic zones. The cost comparisons for the same building between the three different seismic zones leads to useful and interesting conclusions.

## 2 ANALYTICAL RESEARCH

### 2.1 Construction description

The floor plan of the building has dimensions 25 x 25 m, therefore the total area of the floor plan is equal to  $E = 625.00 \text{ m}^2$  (Figure 1). The height of the floors is  $h = 3.00 \text{ m}$ , except for the height of the first floor (ground floor) which is  $h = 4.50 \text{ m}$ . Therefore, the total height of the building is  $h_{\text{tot}} = 16.5 \text{ m}$ . Rigid supports are used and the effect of soil is neglected [21], [22].

The main element of the load-bearing structure can be characterized as the main core, which is located in the center of the building and includes the elevators and stairwells. Regarding the dimensions of the structural elements, there are some small differences from floor to floor. There are also some structural walls in the building. These are the structural walls  $T_3$  and  $T_{10}$  at the two sides of the building's plan. Finally, in terms of beams, they are divided into perimeter and internal. The dimensions of the perimetric beams and the beams of the core are 25 x 70 cm and the internal ones have dimensions 25 x 60 cm. The cross-sections of the structural elements are shown in Table 1.

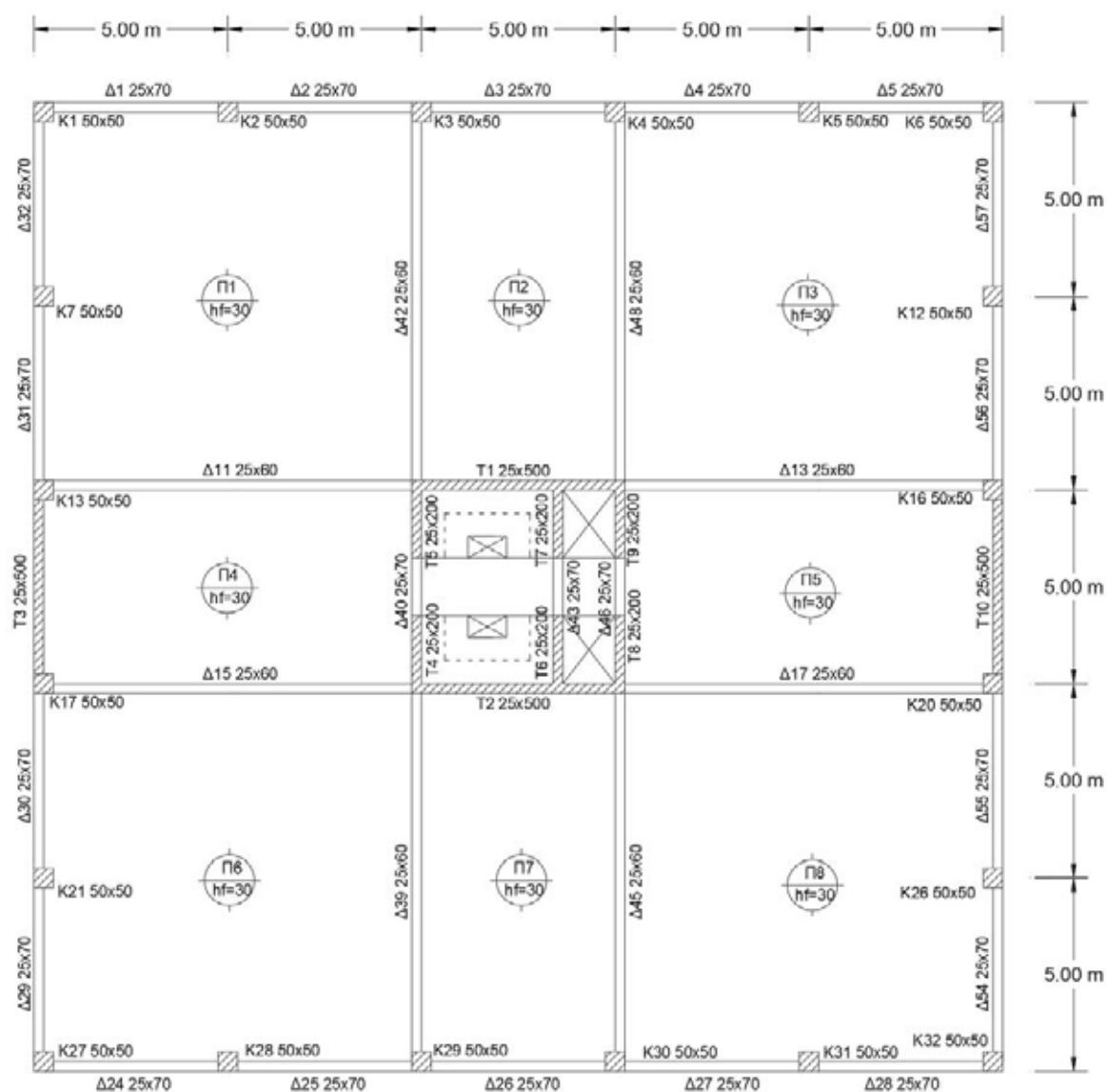


Figure 1: Typical floor plan.

Floor	Height (m)	Beam dimensions (cm)		Wall thickness (cm)	Column dimensions (cm)
		Perimetric	Internal		
1 <sup>st</sup> (Ground floor)	4.50	25x70	25x60	25	50x50
2	3.00	25x70	25x60	25	50x50
3	3.00	25x70	25x60	25	45x45
4	3.00	25x70	25x60	25	40x40
5	3.00	25x70	25x60	25	35x35

Table 1: Dimensions of the structural elements.

## 2.2 Materials

For all the load-bearing structural elements of the construction, concrete quality C30/37 and steel quality B500C were used for the reinforcement bars. According to Eurocode 2 [23], for concrete quality C30/37, the modulus of elasticity is given equal to  $E_{cm} = 32$  GPa. The Poisson ratio is considered equal to zero ( $\nu = 0$ ) for cracked. The steel quality B500C has a characteristic strength equal to  $f_{yk} = 500$  MPa.

## 2.3 Analysis method

The building was analyzed for the vertical loads applied under the combination of  $1.35G + 1.50Q$ , as well as for the seismic actions under the combination of  $G + \psi_2 Q \pm E$ . The dynamic spectral method was used for the dynamic analysis of the building. The building was analyzed and examined in three different seismic hazard zones. In zone I with maximum seismic horizontal ground acceleration  $a_g = 0.16g$ , in zone II with  $a_g = 0.24g$  and in zone III with  $a_g = 0.36g$  (where  $g$  is the acceleration of gravity and is equal to  $9.81 \text{ m/sec}^2$ ). Also, the design spectrum was used, according to Eurocode 8 [24], for soil category B and spectrum type 1. Spectrum data used according to EC8 are displayed in Table 2:

SPECTRUM DATA EC8		
N/A	Type	Data
1	Spectrum type	Horizontal design spectrum type 1
2	Soil category	B
3	Factor $\beta$	0.20
4	Seismic acceleration factor $\alpha$	For the three categories: $\alpha = 0.16, 0.24, 0.36$
5	Gravity acceleration $g$	$9.81 \text{ m/sec}^2$
6	Coefficient behavior $q$	Calculation based on EC8

Table 2: Spectrum data used for the dynamic analysis.

## 2.4 Gravity loads

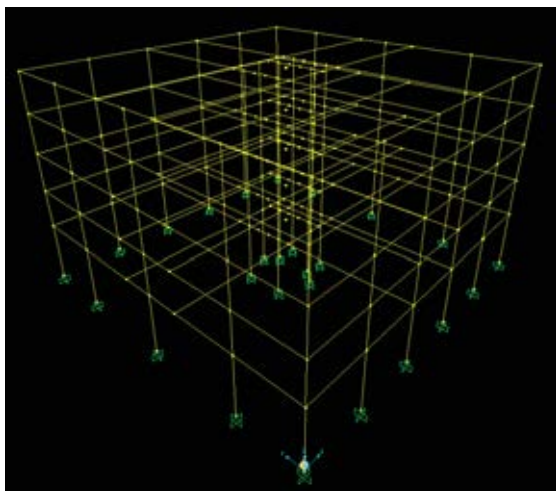
The weight of the reinforced concrete is considered equal to  $25.00 \text{ kN/m}^3$ . The load of the partition masonry is considered to be evenly distributed over the entire surface of the floor plan and the load of the perimeter masonry is applied only on the perimeter beams and directly on them. Also, on the roof, all around the perimeter is considered to be a parapet with a height equal to  $0.90 \text{ m}$ . Flooring is considered to be equal to  $1.40 \text{ kN/m}^2$ . The permanent load for the masonry structures is taken equal to  $1.00 \text{ kN/m}^2$  for the internal brick structures used as partitions and equal to  $8.00 \text{ kN/m}$  for the masonry structures at the perimeter of the slab of the building. The roofing is considered equal to  $3.50 \text{ kN/m}^2$  and the load for the parapet which is at the perimeter of the roof is assumed as equal to  $3.60 \text{ kN/m}^2$ . Live loads are considered equal to  $2.00 \text{ kN/m}^2$  at every floor slab; meaning for the ground floor, the other typical floors and the roof. Permanent and live loads are shown at Table 3.

PERMANENT LOADS		
N/A	Type	Value
1	Flooring	1.40 kN/m <sup>2</sup>
2	Partition brick structures	1.00 kN/m <sup>2</sup>
3	Perimeter brick structures	8.00 kN/m
4	Roofing	3.50 kN/m <sup>2</sup>
5	Parapet roof load	3.60 kN/m <sup>2</sup>
LIVE LOADS		
N/A	Type	Value
1	Ground floor	2.00 kN/m <sup>2</sup>
2	Typical floors	2.00 kN/m <sup>2</sup>
3	Roof	2.00 kN/m <sup>2</sup>

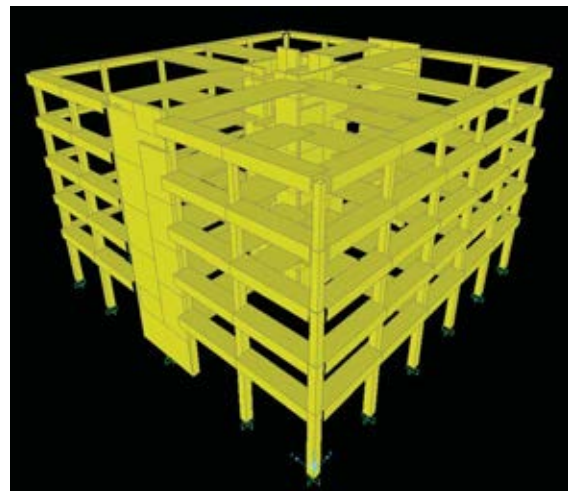
Table 3: Permanent and live loads.

## 2.5 Modelling and dimensioning

Some assumptions were used in the design of the model of the five-storey building. Stiffness for cracked sections is considered equal to 0.5. Torsional stiffness is considered equal to 0.1. For the calculation of the masses of each floor, half the masses of the vertical structural elements of the underneath floor and half the masses of the vertical structural elements of the upper floor were used. In the context of this study, the dimensioning of the individual structural elements was carried out exclusively for the first floor (ground floor) of the five-storey building, for each of the three seismic zones. Figure 2 shows the 3D model of the building. Figure 3 displays the methodology with which the slab loads are transferred to the beams.



(a)



(b)

Figure 2: Views of the 3D building model: (a) Linear finite elements (b) Sections.

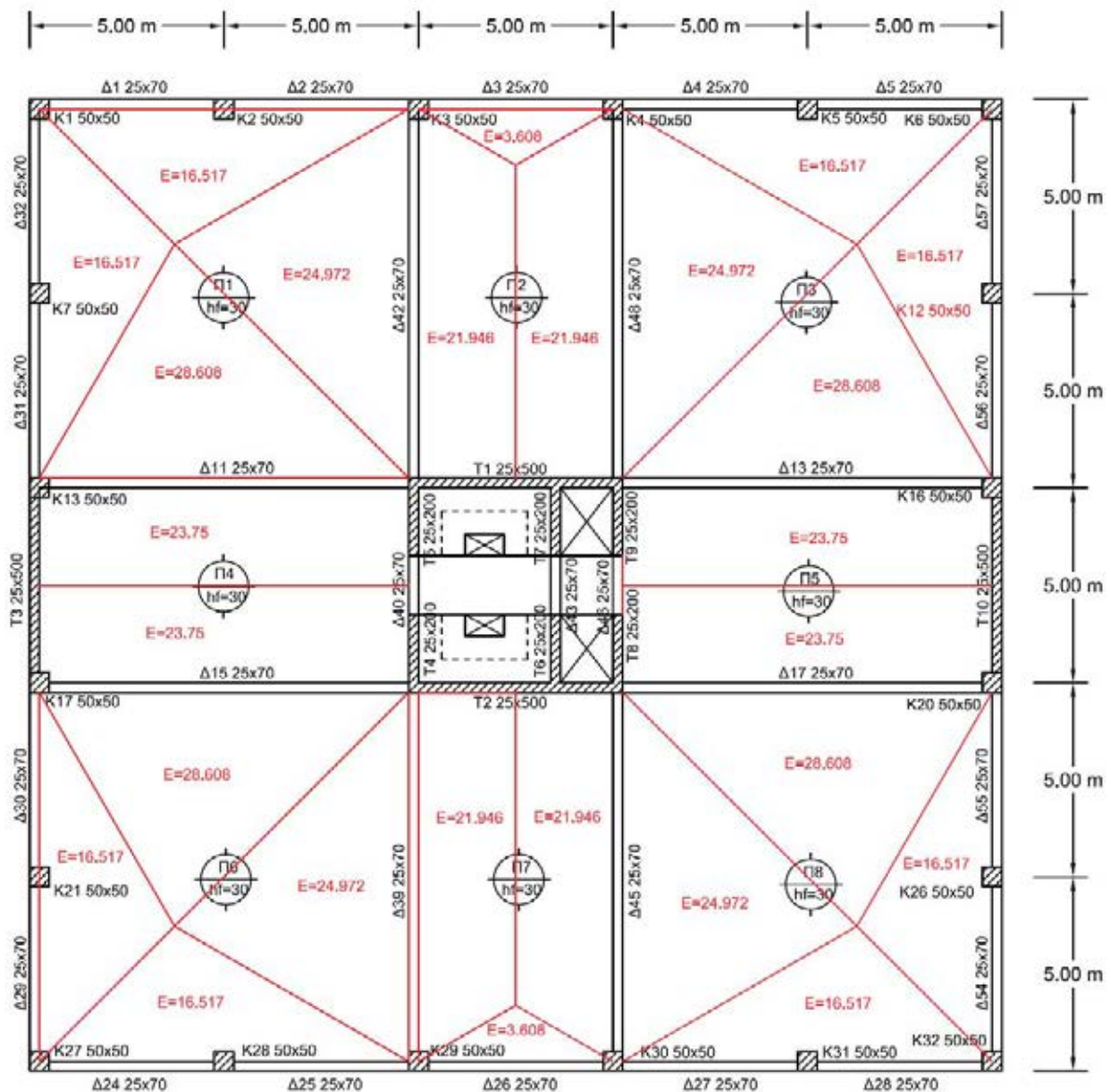


Figure 3: Methodology of calculating beam loads.

### 3 MEASUREMENTS OF MATERIALS

#### 3.1 Concrete and steel measurements for the ground floor

Concrete and steel used for the reinforcement of the structural elements are measured for the ground floor. Concrete is measured in terms of volume and reinforcement steel is measured in terms of weight. Table 4 displays the amount of concrete occupied by the structural elements of the load-bearing structure for all three seismic zones. Also, the same table displays the weight of steel used for all three seismic zones, too. Furthermore, the steel over concrete ratio is calculated and the increase of the steel weight is given in terms of percentages, again for all three seismic hazard zones.



GROUND FLOOR					
Seismic zone	Concrete volume (m <sup>3</sup> )	Steel weight (kg)	Steel / concrete ratio (kg/m <sup>3</sup> )	Increase of steel weight (%)	
Zone I	248.325	19721.91	79.42	-	
Zone II	248.325	21202.56	85.38	7.51	
Zone III	248.325	22360.64	90.05	13.38	5.46

Table 4: Concrete and steel measurements for ground floor.

### 3.2 Concrete and steel measurements for the whole building

The measurements of the materials calculated for the ground floor are used for the estimation of the quantities of the concrete and steel needed for the whole load-bearing structure of the building. Table 5 shows the results for the quantities of concrete and steel for the whole building structure.

BUILDING					
Seismic zone	Concrete volume (m <sup>3</sup> )	Steel weight (kg)	Steel / concrete ratio (kg/m <sup>3</sup> )	Increase of steel weight (%)	
Zone I	1151.58	93636.64	81.31	-	
Zone II	1151.58	99738.59	86.61	6.52	
Zone III	1151.58	105118.39	91.28	12.26	5.39

Table 5: Concrete and steel measurements for building.

## 4 ANALYSIS OF RESULTS

### 4.1 Concrete and steel measurements for the ground floor

The ratio of reinforcement steel used for the rebars over the concrete volume used for concreting the structural elements of the load-bearing structure is calculated for all three seismic hazard zones both for ground floor and for the whole building (Figure 4). Moreover, the reinforcement steel weight increment when changing seismic zone is calculated, too. This calculation takes place for changing from zone I to zone II, from zone I to zone III and from zone II to zone III both for the ground floor, as well as, for the whole building (Figure 5).

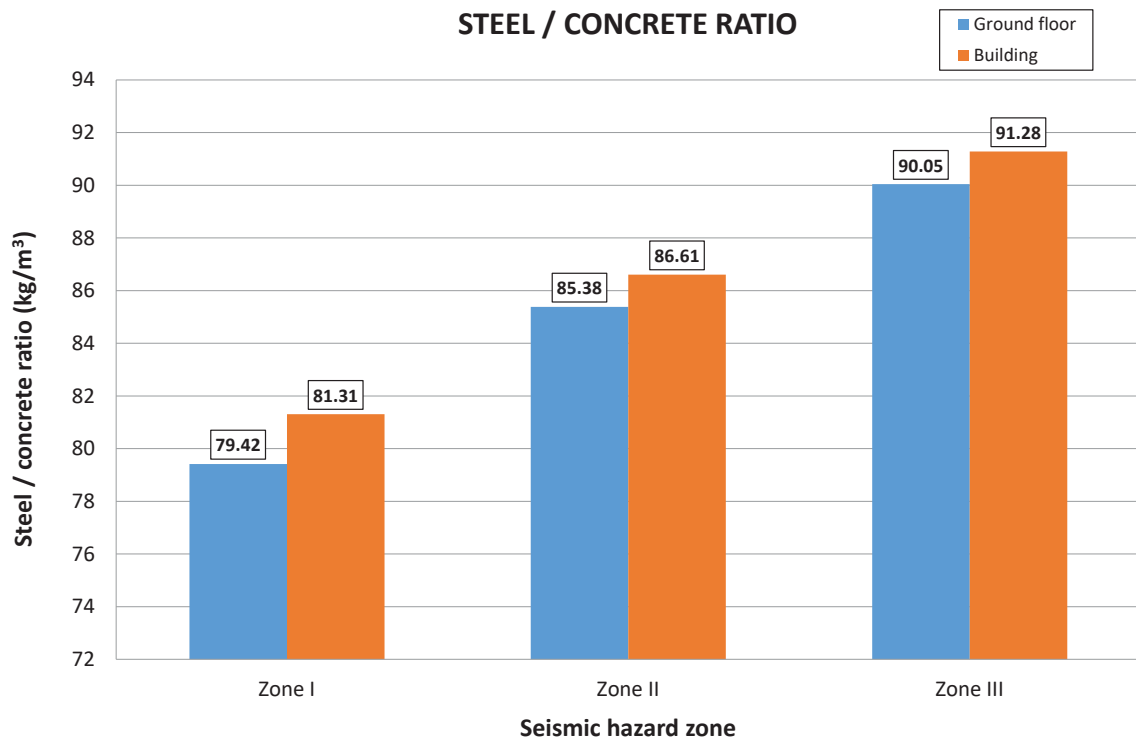


Figure 4: Steel / concrete ratio diagram for the ground floor and the whole building.

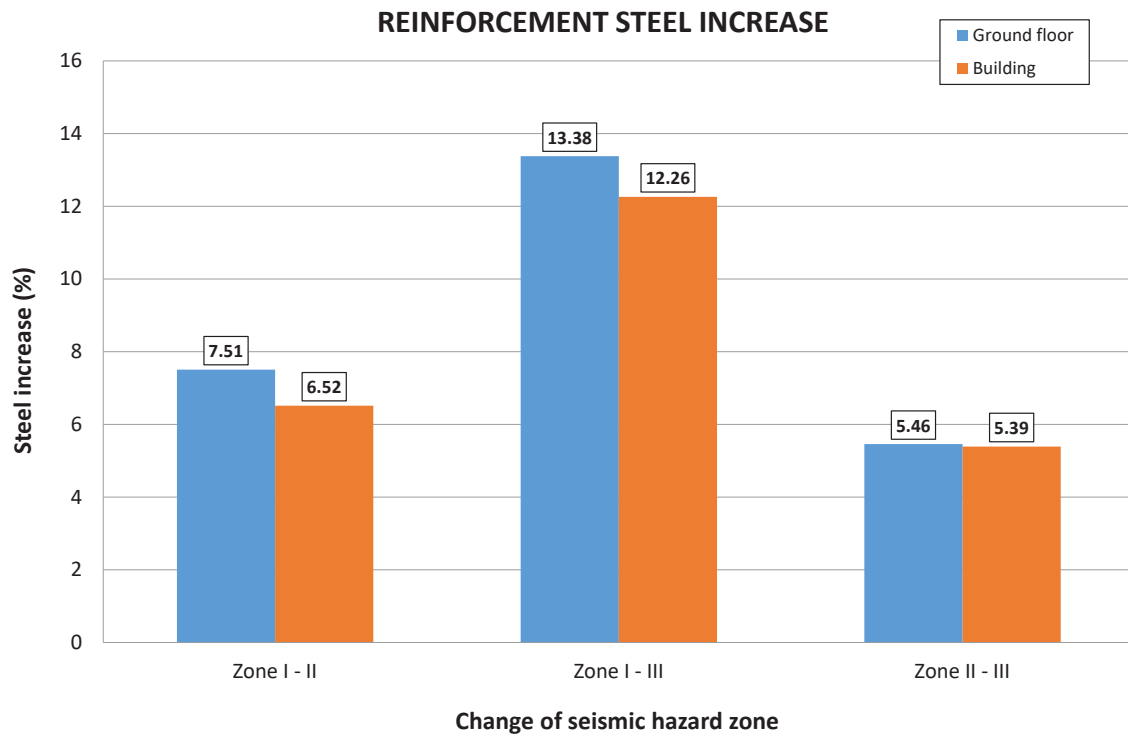


Figure 5: Diagram of steel increase when changing seismic zone for the ground floor and the whole building.



## 4.2 Analysis of results

The analysis of the previous results leads to the following:

1. As far as the floor slabs are concerned, both the volume of their concrete and the weight of their steel do not change in the three seismic hazard zones.
2. Collectively, in terms of reinforcement steel weight, there is an increase of 6.52% from seismic zone I to II and 5.39% from seismic zone II to III (Figure 5). The increase rates of the steel weight for the ground floor of the building are similar, 7.51% and 5.46% respectively (Figure 5).
3. Also, Table 5 and Figure 4 show that the requirement of the five-storey building in reinforcement in seismic zone I is 94 tn with steel to concrete ratio equal to  $81.31 \text{ kg/m}^3$ , while for zone III the weight of reinforcement reaches 105 tn with a ratio of steel to concrete equal to  $91.28 \text{ kg/m}^3$ .

## 5 CONCLUSIONS

The observation of the measurement tables of the concrete volume and those of the steel weight of the various structural elements of the building in question, as well as the tables and the various diagrams concerning the steel/concrete ratio and the percentage increase of the weight of steel leads to some conclusions that mainly concern the behavior of the structural elements but also the whole construction in the three seismic hazard zones and consequently the cost that will be spent for this construction.

1. From seismic zone I to zone II, there is an increase in seismic acceleration of 50%, from I to III 125% and from II to III 50%. These percentages should be compared mainly with the percentages of increase in the weight of steel, in order to prove if the construction cost of the building is within reasonable limits.
2. The sizing of the slabs, whether it concerns the reinforcement (steel weight) or the cross sections (volume of concrete) remains constant in all three seismic zones. Therefore, the ratio of steel to concrete in the slabs also remains constant for all floors and finally throughout the construction.
3. Regarding the whole construction, as it is logical, as the weight of the reinforcement increases separately for each structural element, moving from one seismic zone to another, the same increases for the whole construction. This change plays a very important role, as with the increase of the weight of the reinforcement, there is a corresponding increase of the cost of the structure. However, the total increase in the quantity of materials and consequently the construction cost from seismic zone I to II is only of the order of 6.52%, i.e., 8 times less than the increase in seismic acceleration in the respective zones. Also, the increase in the amount of materials from seismic zone I to III is of the order of 12.26%, i.e., 10 times less than the increase in seismic acceleration in these zones. Finally, the increase in the amount of materials from seismic zone II to III is of the order of 5.39%, i.e., 9 times smaller than the increase in seismic acceleration in the respective zones.
4. In conclusion, observing the results obtained for all the structural elements in the three seismic zones, it can be said that the rate of increase of construction costs from one zone to another is quite small in relation to the rate of increase of seismic acceleration in the respective seismic hazard zones. Thus, if the engineer wishes, for reasons of greater safety, to dimension a construction, using the immediately larger seismic zone than the one in which the construction is actually located, he can do so without significantly increasing the cost of materials (6.52% from seismic zone I to II and 5.39% from seismic zone II to III). The same could be said for the case where the building is

located in the seismic hazard zone I and the engineer wishes to dimension it in zone III. The rate of increase of the cost of materials (12.26%) is less than the safety that thus ensures the engineer for the relevant structure.

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